

those previously used; 10 per cent. of water by weight was used in each case, but the briquettes were  $1\frac{1}{2}$ " by  $1\frac{1}{2}$ " (or  $2\frac{1}{4}$  square inches in section,) prepared with the same cement as that previously used ( $q^2$  in table C) and reduced to the square inch strain.

It will be noticed that, notwithstanding these facts, the strains obtained from No. 1, both at 7 and at 28 days, differs from those already recorded at those periods when made with the 1" by 1" moulds (*vide*  $q^2$  tests in table C). This appears to point to the fact that the smaller briquettes can be made more dense and uniform in texture than those of larger size, and consequently afford better results in testing.

### 3 TO 1 TESTS: COMPARATIVE STRENGTH BY WEIGHT AND BY VOLUME.

| No. | By weight at |          | Per-centage of increase from 7 to 28 days. | By volume at |          | Per-centage of increase from 7 to 28 days. | Extent to which strength is decreased when proportions are by volume instead of by weight, at |           |
|-----|--------------|----------|--|--------------|----------|--|---|-----------|
|     | 7 days.      | 28 days. |  | 7 days.      | 28 days. |  | 7 days.   | 28 days.  |
|     | lbs.         | lbs.     |  | per cent.    | lbs.     |  | lbs.  | per cent. |
| 1   | 145          | 182      | 25.5                                       | 131          | 159      | 59.0                                       | 10.35   | 12.17     |
| 2   | 127          | 170      | 25.2                                       | 107          | 131      | 87.1                                       | 15.20   | 22.94     |
| 3   | 143          | 244      | 41.3                                       | 105          | 172      | 63.8                                       | 26.50   | 29.50     |
| 4   | 113          | 214      | 89.3                                       | 82           | 155      | 89   | 27.60   | 27.50     |
| 5   | 178          | 245      | 37.6                                       | 119          | 177      | 48.7                                       | 33.10   | 27.70     |
| 6   | 221          | 330      | 33.0                                       | 143          | 218      | 34.4                                       | 35.20   | 33.90     |

An attempt was also made to obtain the relative strengths of concrete made entirely of bluestone aggregates, and that made with river gravel and sand, but with hardly satisfactory results, in consequence of the size of the blocks being too large.

The blocks were made in each instance 6 inches in thickness, 9" by 9" on the surface, and were gauged 6 to 1 (by volume) of aggregate and cement, with 6.4 per cent. of water for the bluestone concrete, and 5.06 per cent of water for the gravel and river sand mixture.

The "bluestone" aggregate was composed of equal parts of 1" and 2" metal, mixed with 50 per cent. of screening passing through a  $\frac{1}{4}$ ", but not through an  $\frac{1}{8}$ " mesh, and of bluestone dust in the proportion of 1 to 2. The weight of this mixture was 121.5lbs. per cubic foot.

The "gravel and sand" aggregate consisted of gravel ranging from  $\frac{1}{2}$  inch to 2 inches in gauge, mixed with Nepean River sand in the proportion of  $2\frac{1}{2}$  to 1, and weighed 129lbs. per cubic foot.

The same cement was used for both concretes, and three blocks of each kind were made, and sent to Professor Warren's testing room at the Sydney University, to be tested for compression when the concrete was 21 days old, half of which time was under water. Professor Warren, who kindly undertook the test, reported that they presented too large an area for the machine, which is limited to a pressure of 100,000lbs.

One bluestone block cracked *on one side* at 67,000lbs., but there was no sign of crushing at 100,000lbs.; the second did not crack even at 100,000lbs.; and the third was not attempted.

One Nepean gravel block cracked at 54,000lbs., and crushed at 85,000lbs.; the second cracked at 96,000lbs.; but the third did not even crack at 100,000lbs.

The results appear to be in favour of the bluestone concrete, but are not satisfactory; and further experiments with smaller blocks will be made shortly to settle the point accurately.

Several attempts have been made to manufacture Portland cement in the colonies, and a good deal of money has been spent in experiments without much success; the apparent difficulty being to obtain the class of lime that will produce the necessary chemical change—effected during calcination when the lime is mixed with silica and alumina—whereby the carbonates are transferred into silicates of lime.

The author has himself been present at several of these trials, which have resulted in failure, either from the fact of the materials which were employed not possessing the proper chemical constituents, or from defective manufacture. Under these circumstances it may be supposed that he feels pleasure in stating that he has just had his attention drawn to a sample of cement made in Tasmania from materials obtained within some twelve miles of Hobart, which has been exhibited at the recent exhibition held under the auspices of this Association, and which he is now testing. Although, up to the present, the tests have only reached the seven day period, and the ultimate behaviour of the material has still to be cautiously observed, it will doubtless be of interest to inform the members present that—so far—the prospects of this being a genuine and valuable cement

appear to be very good. The tensile strength of the neat cement at 3 and 7 days was 421 and 693lbs. per square inch respectively; and the test of the 3 to 1 briquette at 7 days gave a result of 213lbs. per square inch, which may be regarded as indicative of considerable initial strength. The pats gave no sign of "blowing" or cracks, and the color, which is light grey, is a good tint.

The small parcel submitted to the author hardly justifies the formation of an opinion of the general fineness and weight of the cement; that which was sieved gave a residue of only 1.58 per cent. on the A sieve (of 2,500 meshes to the square inch) which shows it to have been well ground; in all probability it was put through a Chilian mill.

The chemical analysis, by W. A. Dixon, F.I.C. (which has been submitted to the author for his inspection) is of a rather favorable character, being as follows:—

|  |     |     |     |     |     |     |      |
|--|-----|-----|-----|-----|-----|-----|------|
| Lime   | ... | ... | ... | ... | ... | ... | 66.6 |
| Magnesia   | ... | ... | ... | ... | ... | ... | 1.2  |
| Alumina  | ... | ... | ... | ... | ... | ... | 4.7  |
| Silica, free                                     | ... | ... | ... | ... | ... | ... | 1.9  |
| Silica, combined                                 | ... | ... | ... | ... | ... | ... | 19.2 |
| Carbon, combined air and traces of carbonic acid | ... | ... | ... | ... | ... | ... | 3.1  |
| Oxide of Iron                                    | ... | ... | ... | ... | ... | ... | 3.1  |
| Traces sulphuric acid and alkalies               | ... | ... | ... | ... | ... | ... | 0.2  |

Mr. Dixon also remarks that "the quantity of lime in this cement is somewhat in excess of that usually found, whilst the silica and alumina are deficient. The manufacture has, however, been so carried out that nearly all the silica is in the combined or active cementing condition; indeed, of all cements which have come under my notice, this is the highest, by about one-third, in combined silica. Under these circumstances the cement should be very hard setting, should stand sand well if finely ground."

A comparison of the above analysis with that given by HENRY REID, in his work on the manufacture and use of Portland cement (page 354) as the composition of a good cement, viz:—

|          |     |     |     |     |     |       |           |
|----------|-----|-----|-----|-----|-----|-------|-----------|
| Lime     | ... | ... | ... | ... | ... | 60.05 | per cent. |
| Magnesia | ... | ... | ..  | ... | ... | 1.17  | "         |
| Alumina  | ... | ... | ... | ... | ... | 10.84 | "         |
| Silica   | ... | ... | ... | ... | ... | 24.31 | "         |
| Alkalies | ... | ... | ..  | ... | ... | 1.54  | "         |

will show a tolerably close resemblance between the two, the chief difference being that the Tasmanian sample is evidently "over-limed," which the maker affirms has been intentionally done, possibly with the idea of increasing the immediate strength.

One peculiarity in this cement is that it took 18 hours to set, a much longer time than any ordinary cement requires.

However, there appears to be sufficient merit in this attempt at the manufacture of a colonial cement to warrant us in wishing the speculators in the venture every success in their praiseworthy undertaking.

In conclusion, the author would apologise for the incomplete character of these notes, as the time at his disposal has been restricted, and the experiments in connection with cement are still being carried on; final results cannot therefore be expected at the present time. He trusts, however, that enough has been shown to prove the necessity that exists in Sydney for a careful and intelligent examination of every shipment of cement that is offered for use on important work, regardless of the utterly misleading recommendation of "brands," or the self-satisfied assurance of the "practical" man who will tell you that he can at once pronounce, by the touch, if a cement be good or bad (a mysterious gift which—if reliable—would be of infinite value, and one before which the most scientific chemists would bow the head!)

There is no doubt that, in conjunction with some excellent cement, a lot of inferior and adulterated material is often shipped to Australia, and offered to the public at a cheap rate. Perhaps this has been already rejected at home, and the manufacturer thinks it will do for the colonial market; perhaps it has been under-burnt; or in all probability it has simply been adulterated with a cheaper ingredient, such as free lime, pulverized slag, or shale; or, if a high initial strength is required, about 2 per cent. of plaster of Paris may have been added.

Danger in such cases is to be apprehended; added to which there is the additional risk of injury through bad packing or wet during the voyage, all of which possibilities conspire to make the selection of cement a very anxious matter, unless it receives the consideration of one who has an intelligent understanding of how to set about the work of judging and determining its merits. That all engineers should endeavour to obtain this knowledge is self-evident;



in support of which it is only necessary to quote the following remarks made by MR. (now SIR) JOHN FOWLER in his presidential address before the Institution of Civil Engineers in the year 1866, when enumerating some of the requirements of a civil engineer:—

“Cement is used, chiefly with sand, in various proportions, according to the nature of the work to be executed; and it is not only necessary to possess the requisite knowledge and experience for determining the proper proportions of cement and sand for each individual case, but it is desirable to have the means of determining by direct and repeated experiment the strength and quality of the cement which it is intended to use.”

How much more that applies at the present day when the use of cement has so wonderfully expanded (especially in its application to concrete work), it is unnecessary to say!

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#### APPENDIX A.

### SPECIFICATION

FOR THE SUPPLY OF CEMENT FOR THE USE OF THE MUNICIPAL COUNCIL  
OF THE CITY OF SYDNEY DURING THE YEAR 1886.

*(Clauses relating to Tests.)*

\* \* \* \* \*

“The cement will have to satisfy the following tests, which will be conducted in this office, under the supervision of the City Surveyor or his authorised officer.

“The results of tests made on cement supplied under this contract will be made known to the contractor, if desired by him.

“SPECIFIC GRAVITY and tests for adulteration.—The specific gravity of all cement supplied under this contract must not be less than three and one-tenth (3.10) when carefully tested by approved gravimeter; in addition to which—if the City Surveyor deem it necessary—further tests by chemical treatment may be made, to ascertain if the cement is adulterated by the introduction of any foreign matter. Cement of less specific gravity than the minimum standard of three and one-tenth (3.10), or which shows any indication of having been adulterated, will not be accepted under this contract.

“Weight.—The weight of cement will be determined by filling the standard measure with the cement, allowing it to run in as gently as possible through a specially prepared hopper, to be struck off at surface when full. On no account will it be permitted to press the cement down, or even to allow it to acquire any velocity in its fall to increase its density.

“The cement to be tested will be weighed as received, unsifted, and must weigh at least one hundred and five (105) lbs. per Imperial bushel. It will also be required when sifted, without rubbing, through a sieve of five thousand eight hundred (5800) meshes per square inch, to leave a residue not exceeding twenty (20%) per cent. The sieves used in testing to be those now in use in the testing-room of this office, and known as Adie's standard brass wire sieve, or sieves similar in description to them.

“Proportions of cement, water, and sand to be ascertained by weight and the temperature of the water used, both in the mixing and in the setting-tank, will be noted.

“The cement to be tested will be made into briquettes, both of neat cement, and of cement and sand mixed in the proportion of three (3) parts of sand to one (1) part of cement, with such proportions of water as will be hereafter specified.

“The sand employed in the cement tests to be obtained from crushed sandstone, sifted through a sieve of (400) four hundred meshes per square inch; and to be caught on a sieve of (900) nine hundred meshes per square inch.

“Tensile strength will be ascertained by Adie's testing machine; strain to be applied at the rate of (200) two hundred lbs. per minute.

“The neat cement briquettes, after being thoroughly mixed with from (16) sixteen to (20) twenty per cent. of water, according to the nature of the cement, will be tested at the expiration of (7) seven, and of (28) twenty-eight days from date of mixing, and will be required to stand a strain of not less than (400) four hundred lbs. and (550) five hundred and fifty lbs. per square inch, respectively.

“The briquettes of one (1) of cement to three (3) of sand, after being thoroughly mixed with from nine (9) to (10<sup>0</sup>/<sub>10</sub>) per cent. of water will be tested at (7) seven and (28) twenty-eight days after being made.

“The minimum standard tensile strain at (7) seven days is ‘ninety (90) lbs. per square inch; and at (28) twenty-eight days ‘one hundred and forty-four (144) lbs., provided the neat cement ‘sets in less than (2) two hours, or is what is known as quick setting; ‘but should the neat cement take more than two (2) hours to set, or ‘be what is known as ‘slow setting,’ the minimum standard is ‘(200) two hundred lbs. per square inch.

“To determine its setting properties, the cement, after being ‘mixed neat and made into pats, will be tested with a weight ‘equal to one (1) lb. avoirdupois, pressing on an area of cement ‘under test equal to that of a circle of one-sixteenth ( $\frac{1}{16}$ ) of an inch ‘in diameter. When the pressure produces no depression or inden- ‘tation on the surface, the cement is considered to be set. Neat ‘cement pats kept in air to observe for colour, and others placed in ‘water after setting for seven (7) days, to ascertain fitness for ‘immediate use, and ensure the absence of free lime, will also be ‘applied as may be deemed necessary.

“The above tests are practically similar to those approved by ‘the Harbours and Rivers Department of this colony, and are ‘based upon the official requirements of the London Metropolitan ‘Board of Works, and the rules and regulations for the supply and ‘testing of Portland cement adopted in Germany, Austria, and ‘Russia, being actually lower than the standards therein laid down.

“Any cement that will not satisfy the above tests will not be ‘approved.”

\* \* \* \* \*

“The contractor is to state in his tender the rate at which he ‘will deliver the cement, in accordance with the conditions of this ‘specification, at per cask, containing a net weight of cement, ‘exclusive of cask and packing, of not less than three hundred and ‘eighty (380) lbs. avoirdupois.”

A. C. MOUNTAIN, M. INST. C.E.,

City Surveyor.

Sydney, October 9th, 1885.





APPENDIX B—ENGLISH CEMENTS.

| Reference Nos. | Neat Cement Briquettes—Tensile Strain at |         |          |        |        |         | 3 to 1 Briquettes—Tensile Strain at |          |        |        |         | Weight per bushel. |                   | Residue on Sieves. |       |       | Hours in setting. | Tests for        |                     |
|----------------|--|---------|----------|--------|--------|---------|-------------------------------------|----------|--------|--------|---------|--------------------|-------------------|--------------------|-------|-------|-------------------|------------------|---------------------|
|                | 3 days.                                  | 7 days. | 28 days. | 3 mos. | 6 mos. | 12 mos. | 7 days.                             | 28 days. | 3 mos. | 6 mos. | 12 mos. | As recd.           | Sifted.           | A.                 | B.    | C.    |                   | Expansion.       | Colour.             |
| A 1            | 372                                      | 475     | 605      | ...    | ...    | 601     | 155                                 | 129      | ...    | ...    | ...     | 100.62             | 87 $\frac{1}{4}$  | 17.13              | ...   | ...   | 9                 | puffing at edges | dull brown          |
| B 1            | 496                                      | 604     | 762      | 746    | 809    | 820     | 107                                 | 178      | 207    | 263    | 269     | 107 $\frac{1}{4}$  | 100 $\frac{1}{2}$ | 11.81              | 20.59 | 36.62 | 8                 | no change        | grey tints          |
| " 2            | 350                                      | 422     | 526      | 854    | ...    | ...     | 135                                 | 205      | 269    | ...    | ...     | 109                | 97 $\frac{1}{2}$  | 13.2               | 21.3  | 35.4  | $\frac{3}{4}$     | do.              | do.                 |
| " 3            | 619                                      | 656     | 786      | ...    | ...    | ...     | 151                                 | 218      | ...    | ...    | ...     | 107 $\frac{1}{2}$  | 96 $\frac{3}{4}$  | 13.6               | 21.4  | 36.40 | $\frac{1}{4}$     | do.              | grey and buff tints |
| " 4            | 513                                      | 642     | 712      | ...    | ...    | ...     | 124                                 | 170      | ...    | ...    | ...     | 106 $\frac{3}{4}$  | 95 $\frac{3}{4}$  | 16.3               | 24.5  | 36.90 | $\frac{1}{2}$     | do.              | do.                 |
| " 5            | 413                                      | 462     | 578      | ...    | ...    | ...     | 79                                  | 140      | ...    | ...    | ...     | 106 $\frac{1}{2}$  | 97                | 13.6               | 21.8  | 35.80 | $\frac{1}{4}$     | do.              | do.                 |
| " 6            | 571                                      | 629     | 720      | ...    | ...    | ...     | 119                                 | 186      | ...    | ...    | ...     | 107 $\frac{3}{4}$  | 98 $\frac{1}{2}$  | 14.2               | 21.9  | 35.20 | $\frac{1}{4}$     | do.              | do.                 |
| " 7            | 405                                      | 546     | 598      | ...    | ...    | ...     | 100                                 | 183      | ...    | ...    | ...     | 109                | 102 $\frac{3}{4}$ | 8.8                | 19.0  | 33.80 | $\frac{1}{4}$     | do.              | do.                 |
| " 8            | 546                                      | 608     | 677      | ...    | ...    | ...     | 106                                 | 201      | ...    | ...    | ...     | 103 $\frac{3}{4}$  | 93                | 15.37              | 21.87 | 32.86 | $\frac{1}{2}$     | do.              | do.                 |
| " 9            | 474                                      | 529     | 678      | ...    | ...    | ...     | 97                                  | 189      | ...    | ...    | ...     | 111 $\frac{1}{4}$  | 110.2             | 12.71              | 21.12 | 33.70 | $\frac{3}{4}$     | slight cracks    | do.                 |
| " 10           | 506                                      | 553     | 621      | ...    | ...    | ...     | 73                                  | 155      | ...    | ...    | ...     | 109                | 98.15             | 13.9               | 21.41 | 34.35 | $\frac{3}{4}$     | no change        | do.                 |
| " 11           | 303                                      | 379     | 472      | ...    | ...    | ...     | 99                                  | 171      | ...    | ...    | ...     | 115                | 104.92            | 13.8               | 22.43 | 33.9  | $\frac{1}{4}$     | do.              | do.                 |
| " 12           | 372                                      | 536     | 621      | ...    | ...    | ...     | 82                                  | 142      | ...    | ...    | ...     | 107 $\frac{1}{4}$  | 97 $\frac{3}{4}$  | 11.5               | 21.20 | 33.36 | $\frac{1}{4}$     | do.              | do.                 |
| C 1            | 462                                      | 572     | 628      | 808    | 866    | 850     | 135                                 | 178      | 275    | 302    | 320     | 110                | 101 $\frac{1}{2}$ | 14.96              | 25.17 | 41.7  | 4                 | no change        | light grey          |
| " 2            | 560                                      | 609     | 828      | ...    | ...    | ...     | 218                                 | 262      | ...    | ...    | ...     | 109 $\frac{3}{4}$  | 107 $\frac{1}{2}$ | 3.0                | 9.9   | 27.6  | 1 $\frac{1}{2}$   | do.              | do.                 |
| D 1            | 333                                      | 437     | 551      | 695    | 743    | 689     | 98                                  | 167      | 230    | 261    | 310     | 104 $\frac{1}{2}$  | 90                | 18.64              | 28.14 | 40.91 | 1                 | no change        | brown               |
| E 1            | 388                                      | 417     | 540      | 720    | 662    | 764     | 103                                 | 162      | 270    | 306    | 377     | 102 $\frac{1}{2}$  | 97 $\frac{1}{2}$  | 7.67               | 16.52 | 34.54 | 4 $\frac{1}{2}$   | fine cracks      | brown               |
| " 2            | 532                                      | 603     | 686      | 731    | 744    | 735     | 168                                 | 217      | 321    | 289    | 369     | 103 $\frac{1}{2}$  | 98 $\frac{3}{4}$  | 7.07               | 15.3  | 31.8  | 5                 | slight puffing   | buff and grey tints |
| " 3            | 388                                      | 477     | 585      | 809    | 838    | 846     | 139                                 | 200      | 238    | 302    | 332     | 105                | 97 $\frac{1}{2}$  | 9.9                | 19.4  | 34.3  | 6 $\frac{1}{2}$   | no change        | equal buff and grey |
| F 1            | 381                                      | 509     | 617      | 773    | 841    | 838     | 102                                 | 156      | 299    | 363    | 403     | 109 $\frac{3}{4}$  | 102 $\frac{3}{4}$ | 12.20              | 17.90 | 33.00 | 5 $\frac{1}{2}$   | no change        | equal buff and grey |
| " 2            | 426                                      | 512     | 624      | 770    | ...    | ...     | 80                                  | 155      | 243    | ...    | ...     | 108                | 99 $\frac{3}{4}$  | 8.09               | 14.8  | 28.4  | $\frac{1}{2}$     | do.              | do.                 |
| G 1            | 354                                      | 459     | 610      | 674    | 805    | 922     | 93                                  | 163      | 308    | 331    | 424     | 112                | 105 $\frac{1}{2}$ | 9.2                | 19.00 | 38.10 | 6                 | no change        | buff and grey tints |
| H 1            | 487                                      | 522     | 549      | 745    | 756    | 755     | 156                                 | 218      | 340    | 420    | 469     | 105                | 98 $\frac{3}{4}$  | 5.9                | 12.5  | 28.9  | $\frac{1}{4}$     | no change        | equal buff and grey |
| I 1            | 367                                      | 472     | 556      | 767    | 782    | 798     | 92                                  | 149      | 299    | 372    | 412     | 102 $\frac{3}{4}$  | 95.27             | 8.2                | 17.3  | 32.4  | $\frac{1}{4}$     | no change        | buff and grey tints |
| J 1            | 415                                      | 515     | 594      | 666    | 780    | 823     | 77                                  | 165      | 266    | 336    | 420     | 104 $\frac{1}{2}$  | 99                | 9.9                | 18.7  | 33.7  | 4 $\frac{1}{2}$   | cracks           | buff and grey tints |
| " 2            | 255                                      | 292     | 350      | 560    | ...    | ...     | 51                                  | 125      | 285    | ...    | ...     | 103 $\frac{1}{4}$  | 96 $\frac{1}{2}$  | 9.5                | 18.4  | 34.05 | $\frac{1}{4}$     | no change        | buff                |
| K 1            | 221                                      | 325     | 391      | 531    | ...    | ...     | 44                                  | 96       | 236    | ...    | ...     | 106 $\frac{1}{4}$  | 96 $\frac{3}{4}$  | 13.4               | 21.4  | 35.6  | $\frac{1}{4}$     | no change        | buff                |
| " 2            | 273                                      | 345     | 438      | 752    | ...    | ...     | 88                                  | 183      | 250    | ...    | ...     | 105                | 97                | 10.4               | 20.1  | 34.8  | $\frac{1}{2}$     | do.              | buff and grey tints |
| " 3            | 234                                      | 324     | 402      | 748    | ...    | ...     | 116                                 | 189      | 252    | ...    | ...     | 102 $\frac{3}{4}$  | 94                | 12.8               | 18.9  | 35.0  | $\frac{1}{2}$     | do.              | do.                 |
| " 4            | 261                                      | 364     | 401      | 602    | ...    | ...     | 84                                  | 189      | 243    | ...    | ...     | 105 $\frac{3}{4}$  | 96 $\frac{1}{4}$  | 12.5               | 19.1  | 32.6  | $\frac{1}{2}$     | do.              | do.                 |
| L 1            | 541                                      | 673     | 676      | ...    | ...    | ...     | 153                                 | 225      | ...    | ...    | ...     | 102 $\frac{3}{4}$  | 92                | 13.9               | 21.9  | 32.3  | 1                 | do.              | equal grey and buff |

A. C. MOUNTAIN, M. Instr. C.E.

APPENDIX C—GERMAN AND OTHER EUROPEAN CEMENTS.

| Reference Nos. | Neat Cement Briquettes—Tensile Strain |         |          |        |        |         | 3 to 1 Briquettes—Tensile Strain at |          |        |        |         | Weight per bushel. |         | Residue on Sieves. |       |       | Hours in setting. | Tests for                   |                     |
|----------------|---------------------------------------|---------|----------|--------|--------|---------|-------------------------------------|----------|--------|--------|---------|--------------------|---------|--------------------|-------|-------|-------------------|-----------------------------|---------------------|
|                | 3 days.                               | 7 days. | 28 days. | 3 mos. | 6 mos. | 12 mos. | 7 days.                             | 28 days. | 3 mos. | 6 mos. | 12 mos. | As recd.           | Sifted. | A.                 | B.    | C.    |                   | Expansion.                  | Colour.             |
| A 1            | 187                                   | 280     | 356      | 455    | 488    | 551     | 61                                  | 85       | 160    | 188    | 262     | 91½                | 91¼     | .17                | 2. 5  | 18.21 | 10                | cracks                      | grey                |
| „ 2            | 204                                   | 324     | 480      | 610    | 691    | 730     | 105                                 | 179      | 229    | 337    | 390     | 94                 | 93½     | .08                | 1. 6  | 12. 2 | 6½                | no change                   | grey and buff       |
| „ 3            | 306                                   | 414     | 516      | 638    | 651    | 729     | 116                                 | 172      | 234    | 331    | 345     | 93¾                | 93½     | .21                | 1. 5  | 16. 6 | 7¼                | slight cracking             | grey                |
| B 1            | 714                                   | 811     | 707      | 910    | 714    | 861     | 219                                 | 302      | 319    | 363    | 426     | 102¼               | 93½     | 2.24               | 11. 9 | 35. 6 | 6                 | no change                   | dark grey           |
| „ 2            | 579                                   | 600     | 629      | 830    | 879    | 887     | 143                                 | 265      | 326    | 394    | ...     | 102                | 101¼    | 1. 5               | 6. 3  | 25. 6 | ½                 | do.                         | grey and buff tints |
| „ 3            | 645                                   | 710     | 833      | 815    | ...    | ...     | 163                                 | 268      | 350    | ...    | ...     | 106¼               | 104.1   | 1. 9               | 8. 9  | 31. 0 | ½                 | do.                         | light grey          |
| „ 4            | 663                                   | 735     | 771      | 998    | ...    | ...     | 195                                 | 321      | 315    | ...    | ...     | 106                | 102½    | 2. 3               | 11. 4 | 33. 4 | 2                 | slight cracks               | grey and buff tints |
| C 1            | 492                                   | 521     | 662      | 682    | 789    | 840     | 124                                 | 195      | 252    | 316    | 400     | 96¾                | 92      | 4.26               | 9.74  | 25.   | 7½                | no change                   | dark grey           |
| „ 2            | 488                                   | 573     | 578      | 753    | 776    | 821     | 144                                 | 203      | 304    | 319    | 408     | 99¼                | 93½     | 4. 2               | 9. 8  | 22. 5 | 7                 | do.                         | do.                 |
| „ 3            | 418                                   | 473     | 572      | 722    | 829    | 816     | 116                                 | 185      | 269    | 317    | 382     | 98¾                | 93½     | 5. 8               | 12.05 | 27.24 | 7½                | do.                         | do.                 |
| „ 4            | 429                                   | 500     | 634      | 745    | 778    | 792     | 139                                 | 206      | 231    | 296    | 339     | 95¼                | 89½     | 3. 6               | 8. 2  | 22.   | 6½                | do.                         | do.                 |
| „ 5            | 409                                   | 538     | 694      | 758    | 775    | 876     | 104                                 | 149      | 356    | 428    | 509     | 99                 | 93.6    | 1. 4               | 4. 2  | 16. 6 | 1                 | do.                         | buff and grey tints |
| „ 6            | 488                                   | 705     | 726      | 839    | 853    | 848     | 196                                 | 280      | 405    | 470    | 506     | 102                | 98.5    | .28                | 2. 1  | 14. 9 | 5½                | cracks                      | do.                 |
| „ 7            | 491                                   | 770     | 853      | ...    | ...    | ...     | 148                                 | 257      | ...    | ...    | ...     | 100                | 97.9    | 1.18               | 8.02  | 22. 5 | 4¼                | do.                         | light grey          |
| D 1            | 240                                   | 322     | 402      | 490    | 547    | 607     | 64                                  | 126      | 244    | 291    | 354     | 96¾                | 95¾     | 1. 9               | 8.18  | 22.98 | 10                | cracks and puffing at edges | brown               |
| „ 2            | 285                                   | 388     | 430      | 527    | 640    | 679     | 87                                  | 134      | 220    | 290    | 405     | 96¼                | 94½     | 3. 2               | 10.   | 24. 8 | 8½                | no change                   | buff and grey tints |
| E 1            | 573                                   | 575     | 712      | 746    | 760    | 882     | 185                                 | 182      | 267    | 328    | 317     | 103¼               | 103     | . 9                | 7.81  | 32. 5 | 5                 | no change                   | brownish grey       |
| F 1            | 402                                   | 435     | 599      | 744    | 770    | 820     | 99                                  | 157      | 331    | 360    | 427     | 97¼                | 92¾     | .82                | 7. 4  | 23. 2 | ¾                 | no change                   | grey and buff       |
| „ 2            | 338                                   | 520     | 608      | 801    | 824    | 792     | 128                                 | 188      | 256    | 381    | 451     | 94¾                | 90½     | . 2                | 3. 8  | 21. 8 | 1                 | do.                         | grey                |
| G 1            | 165                                   | 237     | 335      | 370    | 541    | 621     | 49                                  | 88       | 185    | 275    | 351     | 98½                | 97½     | .28                | 1. 9  | 16. 1 | 7                 | cracks                      | buff and grey       |
| H 1            | 307                                   | 491     | 606      | 702    | 729    | 686     | 127                                 | 202      | 271    | 356    | 473     | 101                | 96¼     | 2. 1               | 5. 9  | 18. 3 | 7¼                | no change                   | light grey          |
| I 1            | 427                                   | 557     | 648      | 764    | 822    | 826     | 125                                 | 207      | 371    | 426    | 468     | 101¼               | 95½     | .07                | 2.    | 19. 9 | ¾                 | no change                   | grey and buff       |
| J 1            | 363                                   | 613     | 775      | 804    | 909    | 904     | 114                                 | 170      | 292    | 351    | 374     | 111.25             | 101.19  | 13.12              | 24.26 | 42. 8 | 6½                | no change                   | grey and buff       |
| K 1            | 307                                   | 491     | 606      | 702    | 729    | 765     | 127                                 | 202      | 271    | 356    | 457     | 101                | 96¼     | 2. 1               | 5. 9  | 18. 3 | 7¼                | no change                   | light grey          |
| L 1            | 305                                   | 469     | 572      | 694    | 754    | 772     | 104                                 | 166      | 259    | 354    | 384     | 101½               | 101¼    | 1.02               | 4.42  | 19. 6 | 7¼                | no change                   | buff and grey       |
| „ 2            | 377                                   | 456     | 613      | ...    | ...    | ...     | 100                                 | 144      | ...    | ...    | ...     | 103¼               | 102¼    | .42                | 3. 9  | 23. 7 | 6½                | do.                         | do.                 |
| „ 3            | 401                                   | 460     | 614      | ...    | ...    | ...     | 142                                 | 189      | ...    | ...    | ...     | 109¼               | 109¼    | .24                | 2. 4  | 20. 5 | 4½                | do.                         | do.                 |
| „ 4            | 318                                   | 427     | 576      | ...    | ...    | ...     | 89                                  | 151      | ...    | ...    | ...     | 110                | 107¾    | .28                | 3. 3  | 23. 7 | 6                 | do.                         | light grey          |
| M 1            | 116                                   | 270     | 388      | 590    | 675    | 729     | 38                                  | 96       | 185    | 269    | 321     | 101                | 93¾     | 4.05               | 12. 1 | 26. 9 | 3¼                | no change                   | grey and buff       |
| „ 2            | 326                                   | 457     | 566      | 748    | 827    | 837     | 97                                  | 172      | 273    | 325    | 387     | 102                | 99¼     | 2. 8               | 11. 1 | 28. 4 | 1¼                | do.                         | light grey          |
| „ 3            | 370                                   | 465     | 516      | 636    | ...    | ...     | 77                                  | 131      | 278    | ...    | ...     | 101½               | 97½     | 4.25               | 14. 5 | 29. 4 | 1¼                | do.                         | dark grey           |
| N 1            | 352                                   | 398     | 463      | 656    | 710    | 830     | 50                                  | 106      | 196    | 265    | ...     | 109¾               | 101¼    | 12. 9              | 23. 3 | 37. 7 | 2                 | no change                   | buff and grey       |
| „ 2            | 258                                   | 306     | 431      | 582    | 695    | ...     | 57                                  | 115      | 217    | 276    | ...     | 107                | 97½     | 12. 1              | 19. 8 | 33. 9 | 1¼                | slight cracks               | buff                |
| O 1            | 468                                   | 514     | 609      | 699    | ...    | ...     | 185                                 | 225      | 313    | ...    | ...     | 98½                | 96½     | 3. 2               | 8. 5  | 20. 9 | 1¼                | no change                   | grey                |
| P 1            | 525                                   | 565     | 672      | 813    | ...    | ...     | 187                                 | 308      | 338    | ...    | ...     | 104½               | 100¼    | 2. 2               | 9. 8  | 31. 5 | ¾                 | bad cracks                  | buff and grey       |
| „ 2            | 489                                   | 592     | 675      | ...    | ...    | ...     | 178                                 | 226      | ...    | ...    | ...     | 105¼               | 103¾    | 2. 1               | 10. 3 | 31. 5 | 4                 | no change                   | do.                 |
| Q 1            | 419                                   | 530     | 620      | 799    | 863    | 806     | 142                                 | 235      | 287    | 335    | 392     | 107¼               | 105½    | 1. 9               | 8. 2  | 27. 2 | 2                 | no change                   | light grey          |
| „ 2            | 423                                   | 532     | 738      | ...    | ...    | ...     | 181                                 | 268      | ...    | ...    | ...     | 105¼               | 102½    | 2. 5               | 9. 5  | 26. 3 | 4                 | do.                         | grey, buff tints    |
| „ 3            | 406                                   | 470     | 572      | ...    | ...    | ...     | 172                                 | 262      | ...    | ...    | ...     | 97¼                | 95¾     | 2.39               | 7. 4  | 23. 3 | 3½                | do.                         | light grey          |
| R 1            | 410                                   | 472     | 578      | ...    | ...    | ...     | 131                                 | 199      | ...    | ...    | ...     | 108¼               | 106     | 3. 5               | 13. 0 | 37. 3 | 4                 | cracks                      | buff and grey       |